



Merging treatability results and sustainability assessment: a segregated textile dyehouse effluent

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Abstract

Treatability studies are performed on industrial wastewaters before defining a proper treatment scheme. Segregated effluents are of concern for industrial sectors such as textile, leather, metal etc. where wastewater characterization differs substantially depending on the various processes applied. Conclusions are drawn from the results obtained by checking the removal efficiencies. A treatment train is recommended based on the pollutant removal efficiencies. This type of inadequate evaluation is doomed to fail as it lacks the cross media effects and a whole spectrum of environmental impacts. In this context, the current study targets merging treatability results with the sustainability assessment. A segregated textile wastewater that contains hydrolyzed Reactive Black 5 dye (RB5) is subjected to treatability tests with UV-C activated persulfate (PS) and UV-C activated percarbonate (PC). The results that show 100% RB5 removal are evaluated via life cycle assessment (LCA). By doing so, the treatment alternative that yields minimal environmental impacts is stated. The life cycle assessment methodology used is structured according to the ISO 14040/14044 guidelines. The GaBi software version 7.3 is adopted. The CML is used to estimate the life cycle environmental impacts. The following environmental impact categories are investigated: Global warming potential (GWP), abiotic depletion potential (ADP fossils and elements), acidification potential (AP), eutrophication potential (EP), freshwater aquatic ecotoxicity potential (FAETP), human toxicity potential (HTP), ozone depletion potential (ODP), photochemical ozone creation potential (POCP) and terrestrial ecotoxicity potential (TETP).

Keywords Environmental impacts · Industrial wastewater · Life cycle assessment · Photochemical oxidation · Reactive black 5 dye · Segregated effluents · Treatment

Introduction

The environment has become increasingly polluted as a result of the waste generated through industrial activities. Various natural and synthetic pollutants and heavy metals in wastewater are the major issues due to their negative effects on humans and other organisms (Ahmad et al. 2020, 2021; Akhtar et al. 2021; Briffa et al. 2020).

Treatment schemes for industrial effluents are shaped by referring to the results of treatability and modelling studies (Li et al. 2019; Germirli Babuna et al. 1998a; 1998b; 1999) that yields the lowest treatment costs (Ilhan et al. 2019; Erdogan et al., 2004). For some cases energy neutrality gains importance (Ødegaard, 2016) along with costs. In this sense, pollutant removal efficiencies obtained during treatability investigations together with the financial burdens usually dictate the applicable treatment train. However, such an approach concentrating only on the removal of pollutants yields inadequate conclusions as cross media effects

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covering the whole spectrum of environmental impacts gain importance.

Segregated effluents with substantially different characterizations are produced in certain industrial sectors such as textile, leather, metal etc. as various auxiliaries are added during various operations under different conditions. Textile industry has a very complex nature in terms of the refractory wastewater constituents as quite a number of auxiliary chemicals are involved in the production of a variety of goods (Orhon et al. 2003). This complex nature reflects itself on the treatment schemes prescribed for textile effluents (Karahan et al. 2002; Germirli et al. 1990). Effective industrial effluent management can be achieved by examining the treatment requirements of segregated wastewater streams having different natures (Dulkadiroglu et al. 2002, 2022; Orhon et al. 2002; Dogruel et al. 2003; Koyunluoglu et al. 2006; Arslan-Alaton et al. 2005, 2006; Oktay et al. 2007; Tezgel et al. 2014; Germirli Babuna et al. 2016).

It is a well-known fact that textile finishing mills generate effluents with color. As a consequence, standards with color limitations are developed for textile dyehouse wastewaters and treatment methodologies targeting color removal are adopted. Besides, only certain steps in textile preparation, dyeing and finishing operations produce colored segregated effluents. Proper environmental management dictates not mixing the segregated textile wastewaters containing color with the ones without color and solving the color problem by handling the colored streams separately. Various treatment alternatives are proposed in the literature to remove color in textile wastewaters (Bilińska & Gmurek, 2021; Collivignarelli et al. 2019; Maqbool et al. 2020; Samsami et al. 2020). It should be noted that commercial textile dyes are not toxic, their toxicity values are generally very low. They are only intentionally designed to resist biochemical as well as photolytic/photochemical/chemical degradation. As such, they remain in the treated dyehouse effluent without deterioration and advanced chemical treatment methods/conditions are needed to degrade the dyes/remove color from dyehouse effluent. However, during dye degradation with strong chemical oxidants such as ozone and ozone combined with hydrogen peroxide or ultra violet radiation forming advanced oxidation processes, it might be possible that degradation products which are more toxic than the original dyes (Arslan-Alaton and Akmehmet Balcioglu 2001; Arslan-Alaton 2003; Arslan-Alaton 2012; Bilinska et al. 2016; Freeman and Reife 2003).

The textile industry is a very water- and chemical-intensive industry. This sector is known for its extremely high water consumption ($\geq 1000 \text{ m}^3/\text{d}$), the complexity and variety of dyes, surfactants, sequestering agents, dye auxiliary chemicals, organic/inorganic salts as well as acids/alkalis employed; producing rather difficult-to-treat, problematic waste streams (Grau 1991; Madhav et al. 2018).

Conventional biological (activated sludge, attached growth, either aerobic or anaerobic/anoxic) and physicochemical treatment of textile effluent is routinely practiced, however, with limited success since characteristic pollution parameters of the textile industry such as COD, color and sulphur cannot be removed efficiently (Madhav et al. 2018; Periyasamy et al. 2018). Until now, several physical (adsorption, coagulation-flocculation, precipitation) and chemical (ozonation, wet air oxidation, sonolysis, advanced oxidation with the Fenton's reagent) treatment alternatives have proven to successfully remove color in dyehouse effluents and textile industry wastewater (Elwakeel 2009; Katheresan et al. 2018; Kokabian et al. 2013; Kusvuran et al. 2005). However, their real-scale application/implementation is most of the time economically not attractive and their performance in total and dissolved organic carbon (TOC and DOC) removal is relatively poor compared to color removal. Hence photochemical (mostly UV-C and UV-A-based) activation of oxidants or catalyst materials has recently become a promising alternative to improve biodegradability, remove color, organic carbon and eventually toxicity from textile wastewater (Cisneros et al., 2002; Raju et al. 2008). Among these photochemical advanced oxidation processes, the UV-C activation of peroxides such as persulfate and more recently percarbonate offers several advantages such as ease of operation, superior/efficient organic matter removal accompanied with rapid color abatement and detoxification, no sludge formation, no air emissions and the use of relatively green oxidants, namely peroxides (Fadaei et al. 2021; López Cisneros et al. 2002; Raju et al. 2008). The major operating cost is related to electric energy requirements to run the UV-C (short-UV) lamps, lamp replacement (around 20–30% of the electricity costs) as well as peroxide costs (Fadaei et al. 2021; López Cisneros et al. 2002; Yue-hua et al. 2011).

Speaking for the process chemistry, persulfate (PS) activation with UV-C mainly produces sulfate radicals ($\text{SO}_4^{\cdot-}$), whereas percarbonate (PC) activation with UV-C basically forms hydroxyl ($\text{HO}\cdot$) as well as the more selective bicarbonate/carbonate radicals ($\text{HCO}_3^{\cdot-}/\text{CO}_3^{\cdot-}$) (Bennedsen et al. 2012; Liu et al. 2018; Miao et al. 2015; Yang et al. 2017). These react with dye molecules and dye assisting auxiliary chemicals to ultimately form mineralization end products of the dyehouse effluent ingredients. Bimolecular reaction rate constants are typically in the order of 10^{-6} – $10^{-9} \text{ M}^{-1} \text{ s}^{-1}$ range for dyes and dye auxiliary chemicals (Bennedsen et al. 2012; López Cisneros et al. 2002; Raju et al. 2008). However, the high salinity and alkalinity of dyehouse effluent create a competitive inhibitory environment in the reaction solution and hence negatively affect oxidation efficiencies (Cooper & Zika 1983; Peyton 1993; Pignatello et al. 2006). Thus, process optimization in terms of pH and oxidant concentration is very critical for photochemically-driven advanced oxidation processes.



When applied to a product (Sezginer et al. 2022; Ozsahin et al. 2022), process (Ozkan et al. 2017; 2020) or service, life cycle assessment (LCA) methodology yields fruitful outcomes to envisage the environmental impacts. A wide spectrum of environmental impact categories can be covered ranging from global warming to various ecotoxicities with LCA. Besides, the whole life cycle or a certain life stage can be investigated in terms of impacts via LCA. There are LCA studies performed on treatment systems, such as operation and maintenance of industrial water purification systems (Yalamacilar, et al. 2021); operation of a wastewater treatment plant (Başkurt et al. 2017); construction (Elginöz et al 2019); and operation (Saad et al. 2019) of a water treatment plant. Putting LCA into use during treatability studies is of importance as decisions on treatment units are shaped based on the results of treatability.

In this context, the objective of this study is to develop a roadmap that merges the treatability results with the sustainability assessment. For this purpose, a segregated textile dyebath discharge that contains hydrolyzed Reactive Black 5 dye (RB5) is subjected to treatability tests with UV-C activated persulphate (PS) and UV-C activated percarbonate (PC). The results yielding 100% RB5 removal are evaluated via LCA to find out the treatment alternative with minimal environmental impacts. This research was performed between the years of 2020–2021 in Istanbul, Turkey.

Materials and methods

All the laboratory scale treatability experiments are conducted on simulated segregated textile wastewater. Separate applications of PC and PS together with UV-C are run.

Experimental

Preparation of the spent, reactive dyebath effluent

A spent (exhausted) reactive dyebath effluent was prepared by dissolving the reactive dye Reactive Black 5 (RB5) in $T = 80\text{ }^{\circ}\text{C}$ distilled water and increasing the reactive dye solution's pH values to above 11 ($\approx 11.2\text{--}11.5$) by adding caustic soda (NaOH; 6 N) to the RB5 solution. In this way, complete hydrolysis of RB5 dye was ensured. Caustic soda is frequently being used during the reactive dyeing process to release the vinyl sulphone group and initiate covalent bond formation between the dye molecule's reactive group and the cellulose anions (Reife 2000).

Peroxide/UV-C experiments

The spent reactive dyebath was used in the peroxide/UV-C experiments after 50-fold dilution and pH re-adjustment

to 8.0 with NaOH solutions (0.1 N and 1 N) to mimic the exact composition of a typical reactive dyehouse effluent (RB5 = 20 mg/L; TOC = 5.25 mg/L) after the textile dyeing, rinsing and finishing stages prior to discharge for dyehouse effluent treatment (Reife 2000). The peroxide/UV-C experiments were conducted in a 500 mL-capacity three-neck quartz flask ($h = 10\text{ cm}$; $r = 4\text{ cm}$) where the reaction solution was stirred at 100 rpm to ensure proper mixing and molecular oxygen saturation. The photochemical reaction chamber consisted of a LZC-ORG model (Luzchem Research Inc., Ontario, Canada) photoreactor (dimensions = $32 \times 33 \times 21\text{ cm}$) equipped with a digitally controlled thermometer and a magnetic stirrer. Ten fluorescent UV-C lamps (8 W each) with a total incident light flux of $I_0 = 1.3\text{ W/L}$ measured with a UV-meter were used in the peroxide/UV-C experiments. Prior to the photochemical experiments, sodium percarbonate (SPC) or sodium persulphate (SPS) was added to the reaction solutions and the UV-C lamps were turned on 15–20 min before the start of the experiments to ensure a stable fluorescent UV-C light emission. Samples were taken at regular time intervals to measure color (peak absorbance at 600 nm) and total organic carbon (TOC). The pH was also followed during the experimental runs. The photoreactor set-up and experimental procedure are described elsewhere in more detail (Ozyildiz et al. 2019).

Statistical analysis was carried out for all instrumental measurements (color as peak absorbance and total organic carbon-TOC) as well as the calculation of color removal rate coefficients (in min^{-1}) using MS Office Excel software. Duplicates were assessed for color (peak absorbance) and TOC results. The significance level in all calculations was set as $p < 0.05$.

Life cycle assessment methodology

The life cycle assessment methodology used is structured according to the ISO 14040/14044 guidelines (ISO 2006a, 2006b). The GaBi software version 7.3 (Sphera 2017) is used. The background data is derived from the Ecoinvent 3.1 Database (Ecoinvent 2013).

Aim and scope of the study

The objective of this study is to evaluate the environmental effects of laboratory-scale decontamination studies performed in segregated textile wastewater streams and to determine which method and conditions are the most environmentally sustainable among the various alternatives.

This study focuses on the energy management and chemical usage of oxidation-based wastewater treatment processes. A comparison of potential environmental impact categories is made in the life cycle models based on energy



consumption and different amounts of chemicals used in wastewater treatment experiments.

In this study, “1 m³ treated wastewater” is selected as the functional unit and all inventory data and environmental impacts are evaluated through this functional unit.

As illustrated in Fig. 1, the system boundaries include the production and transportation of chemicals to the facility, as well as the energy consumption used in experiments.

Inventory analysis

The data used in the study were obtained through experimental studies. The experimental results of the laboratory studies are tabulated in Table 1.

As can be seen from the Table 1, Run 1 and 2 yields the same outcome. Because of this, only Run 1 where a lower level of SPS is fed to the system is analysed with LCA. Similarly, among Runs 3 and 4, only Run 3 is selected for LCA as it requires less SPS input to produce the same removal. Besides Run 10 is also not included in LCA, since a similar outcome with lower SPC input is obtained in Run 9. To sum all up, LCA studies are not performed on Runs 2, 3 and 10, as it is possible to get the same output with fewer inputs.

A model for grid electricity in Turkey has been created using the Ecoinvent database (Ecoinvent Database, 2013) regarding electricity generation in Turkey 2019 (TEIAS 2019). The energy production in Turkey used in the study is based on fossil fuels, primarily hard coal (20%), natural gas (19%), lignite (15%) and hydropower (% 22).

Fig. 1 System boundaries for treatment with **a** SPS; **b** SPC

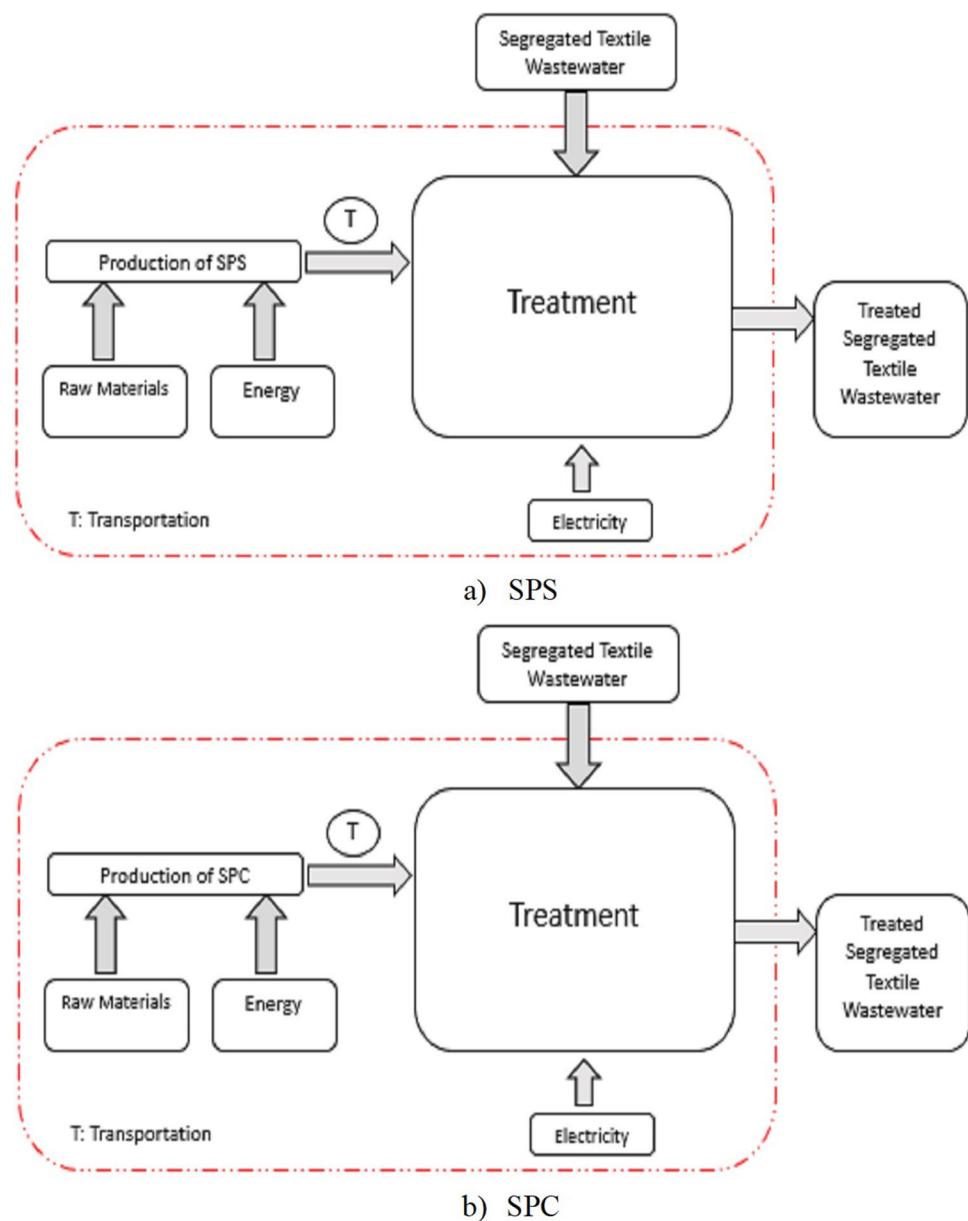


Table 1 Data obtained on treatability studies for a) SPS b) SPC

Run number	SPS concentration (mg/L)	100% Peak absorbance (color) removal time (min)	Electricity requirement (kWh/m ³)
(a)			
1	35.7	60	1.340
2	59.5	60	1.340
3	95.2	30	0.670
4	119	30	0.670
5	238	10	0.223
Run number	SPC Concentration (mg/L)	100% Peak absorbance (color) removal time (min)	Electricity Requirement (kWh/m ³)
(b)			
6	39.25	60	1.340
7	78.5	30	0.670
8	157	20	0.447
9	235.5	15	0.335
10	314	15	0.335

Both of the chemicals used in treatability experiments are imported from China. Transportation distances for the chemicals are calculated using online distance measurements (FreeMapTools 2021) taking into account the location of production. Both SPS and SPC are imported from China, their transportation cover 19,668 km's of sea and 32 km's of highway.

Impact assessment

CML (Center for Environmental Science – University of Leiden, The Netherlands) (Guinee, 2001) methodology is adopted for life cycle impact assessment and the following environmental impact categories are investigated: Global

warming potential (GWP), abiotic depletion potential (ADP fossils and elements), acidification potential (AP), eutrophication potential (EP), freshwater aquatic ecotoxicity (FAETP), human toxicity potential (HTP), ozone depletion potential (ODP), photochemical ozone creation potential (POCP) and terrestrial ecotoxicity potential (TETP).

Results and discussion

The results of the LCA for the experimental runs are tabulated in Table 2.

The factors contributing to the environmental impacts given in Fig. 2 are different for each run. The share of

Table 2 Environmental impacts related to experimental runs

Impact Category	Run numbers							
	1	3	5	6	7	8	9	
ADP elements (kg Sb-equiv.)	1.36E-06	2.89E-06	6.07E-06	1.88E-06	2.17E-06	3.62E-06	5.17E-06	
ADP fossil (MJ)	8.85E+00	6.61E+00	7.32E+00	9.53E+00	6.33E+00	7.01E+00	8.38E+00	
AP (kg SO ₂ -equiv.)	5.66E-03	4.57E-03	5.68E-03	5.95E-03	3.94E-03	4.34E-03	5.19E-03	
EP (kg PO ₄ -equiv.)	3.39E-03	2.02E-03	1.44E-03	3.53E-03	2.07E-03	1.93E-03	2.05E-03	
FAETP (kg DCB-equiv.)	7.86E-01	4.73E-01	3.44E-01	8.19E-01	4.75E-01	4.34E-01	4.57E-01	
GWP (kg CO ₂ -Equiv.)	8.61E-01	5.79E-01	5.41E-01	9.18E-01	5.81E-01	6.06E-01	6.99E-01	
HTP (kg DCB-Equiv.)	5.42E-01	4.04E-01	4.43E-01	5.83E-01	3.83E-01	4.19E-01	4.97E-01	
MAETP (kg DCB-Equiv.)	1.91E+03	1.22E+03	1.01E+03	2.02E+03	1.23E+03	1.22E+03	1.36E+03	
ODP (kg R11-Equiv.)	1.55E-08	4.59E-08	1.04E-07	1.66E-08	1.88E-08	3.12E-08	4.44E-08	
POCP(kg C ₂ H ₄ -Equiv.)	2.87E-04	2.42E-04	3.16E-04	3.09E-04	2.16E-04	2.54E-04	3.14E-04	
TETP (kg DCB-Equiv.)	6.29E-03	4.65E-03	5.05E-03	6.75E-03	4.41E-03	4.77E-03	5.63E-03	

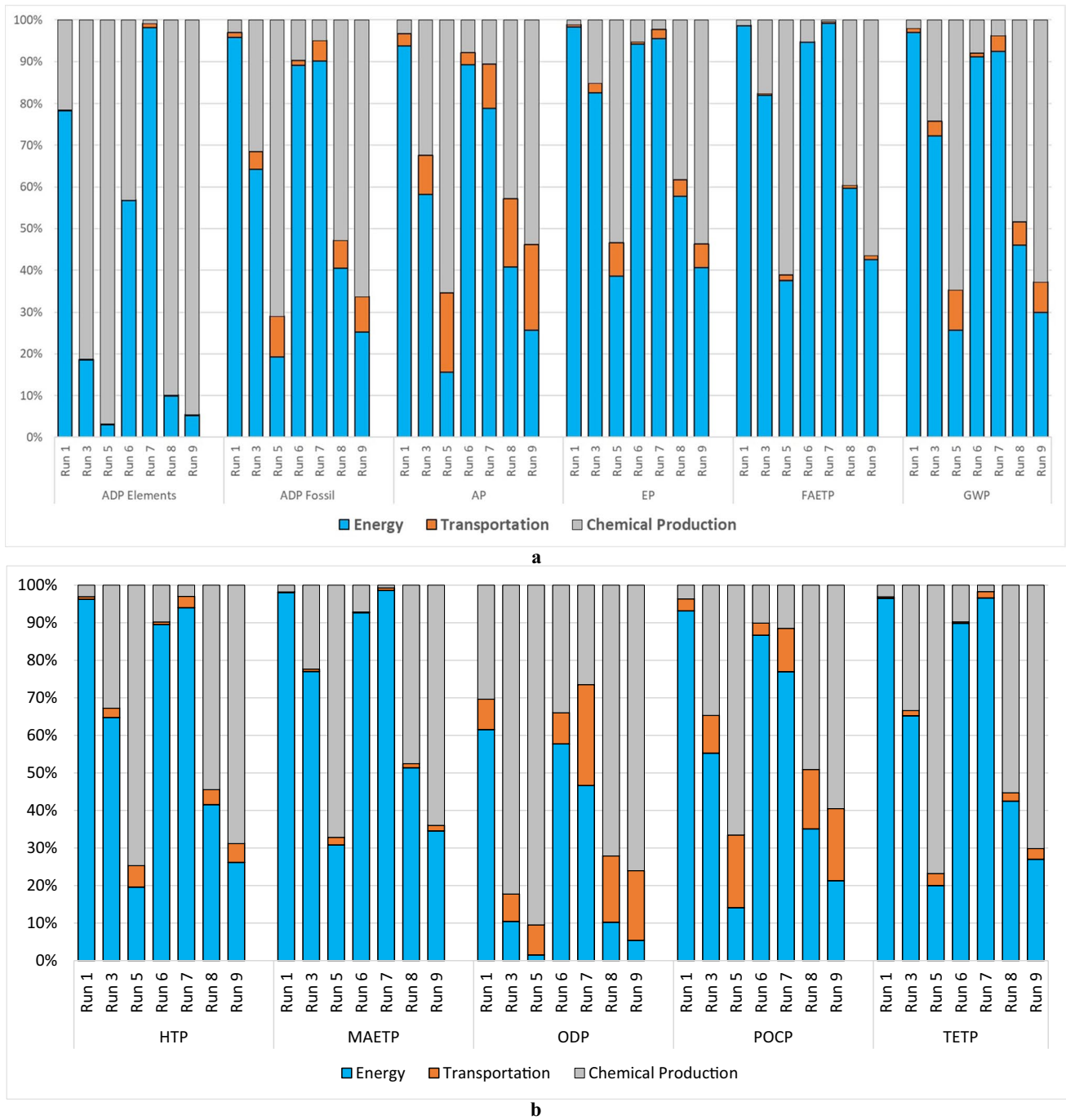


Fig. 2 Contribution of different factors to the total environmental impacts (**a** ADP elements, ADP fossil, AP, EP, FAETP, GWP; **b** HTP, MAETP, ODP, POCP, TETP)

electricity, transportation and chemical inputs in a total impact varies considerably for runs.

As indicated in Fig. 2, for Run 1 electricity requirement dominates ATP fossil, AP, EP, FAETP, GWP, HTP, MAETP, POCP and TETP categories with more than 93% share on the total impacts mentioned. Approximately 78% of ATP elements is of electricity input and 21% from

SPS production for Run 1. ODP of Run 1 is composed of, 61% from electricity, 30% from SPS input and 9% from transportation.

81% of ATP elements for Run 3 is generated by SPS input, where 18% comes from electricity requirement. For Run 3, ATP fossil is due to electricity (64% of the total) and SPS input (32%).

Contributions to AP of Run 3 is electricity (58%), SPS (32%) and the rest of transportation.

Electricity has 82% contribution on EP of Run 3, where 15% comes from SPS input. Similar percentages are also valid for FAETP. About 72 and 24% of GWP are due to electricity and SPS inputs, respectively for Run 3.

HTP of Run 3 is composed of electricity (64%) and SPS (33%) inputs.

About 77 and 23% of MAETP for Run 3 come from electricity and SPS introductions to the system.

SPS and electricity requirements have 82 and 10% shares in ODP of Run 3. On the other hand, 55 and 35% of POCP for Run 3 is composed of electricity and SPS.

TETP is of electricity (65%) and SPS (33%) origin for Run 3.

About 95% ATP elements of Run 5 is generated by SPS requirement. One can find more information on the share of factors for impacts arising from runs in Fig. 2.

Figure 3 illustrates a comparison of the environmental impacts for experimental runs by normalizing the results for Run 1.

Depending on which environmental impact category/categories are of importance, a proper treatment alternative can be quoted. When a detailed comparison between the runs is performed, the following findings arise:

For ADP elements, Run 1 yields the lowest impact. Approximately 115, 350, 40, 60, 170 and 280% elevations are obtained for Runs 3, 5, 6, 7, 8 and 9, respectively in

comparison with Run 1. Therefore, if the level of ADP elements is important for the decision-makers, Run 1 with introducing 35.7 mg/L SPS and 1.340 kWh/m³ energy requirement should be adopted over other experimental conditions.

For ADP fossil category, the lowest unwanted impacts are obtained for Run 3 and 7 with 25 to 28% reductions, namely, than Run 1. Thus, either 95.2 mg/L SPS and 0.670 kWh/m³ energy input (Run 3) or 78.5 mg/L SPC and 0.670 kWh/m³ energy requirement (Run 7) are stated as the optimal results in terms of ADP fossil impact category.

The same AP values are obtained for Runs 1 and 5. The lowest AP arises from Run 7, having 30% reduction in comparison with Run 1. Accordingly, 78.5 mg/L SPC and 0.670 kWh/m³ energy input (Run 7) yields the lowest AP.

Run 1 and 6 generate close EP levels. Similarly Runs 3, 7, 8 and 9 yields approximately similar levels of EP having 40% reductions in comparison with Run 1. The lowest EP can be obtained when experimental conditions of Run 5 is adopted, as 238 mg/L SPS introduction with 0.223 kWh/m³ energy input. In comparison with Run 1, it is possible to reduce EP by 60% with Run 5.

Similar levels of FAETP can be produced by Run 1 and 6. In comparison with Run 1, almost 40% reductions can be achieved with Runs 3, 7, 8 and 9. On the other hand, the lowest FAETP can be obtained with Run 5 where a 65% reduction than Run 1 is observed. Hence 238 mg/l

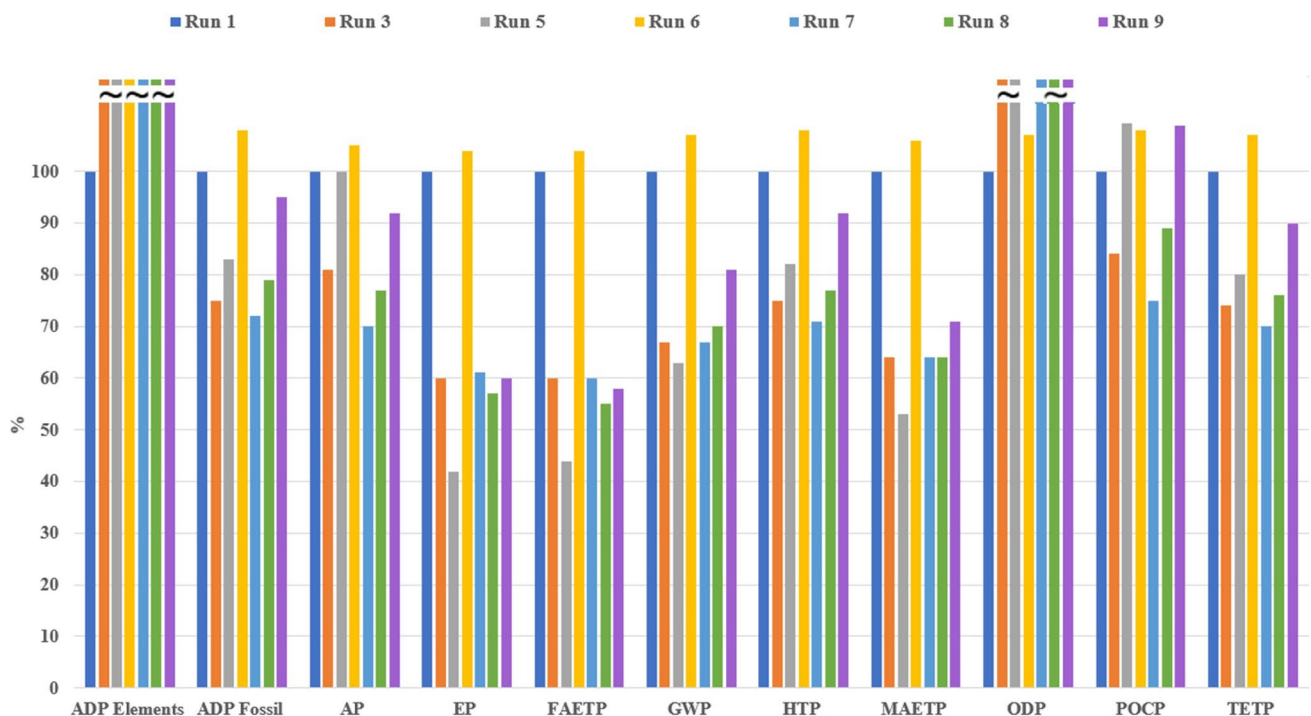


Fig. 3 Comparison of environmental impacts for experimental runs

SPS introduction with 0.223 kWh/m^3 energy input result in the lowest FAETP.

Run 6 results in slightly higher GWP than Run 1. The lowest GWP can be obtained by Run 5 where 38% reduction than Run 1 is getting. Although not as high reduction as Run 5, Runs 3, 7 and 8 have close outputs of GWP with more than 30% lowered GWP than Run 1. Consequently Run 5, involving 238 mg/l SPS introduction with 0.223 kWh/m^3 energy input, can be quoted as the lowest GWP yielding treatment alternative.

In terms of HTP, Run 7 yields the lowest impacts with a 30% reduction when compared with Run 1. Close results to Run 7 are obtained with Run 3 and 8.

For MAETP, almost 47% reduction can be achieved with Run 5 when compared to Run 1. Whereas 35% lower values than Run 1 can be obtained by Run Runs 3, 7 and 8.

All the runs result higher ODP levels than Run 1, however ODP of Run 6 is close to Run 1 with only 7% increase. In comparison with Run 1; 195, 570, 21, 100, 185% elevations are obtained for Runs 3, 5, 7, 8 and 9, respectively.

In comparison with Run 1, almost 10% higher POCP values are achieved for Runs 5, 6 and 9. However the lowest POCP is obtained with Run 7. Run 7 results in 25% reduction when compared to Run 1.

Run 7 yields the lowest TETP as a 30% reduction than Run 1 is obtained. A close result can be seen for Run 3.

As a summary of all the findings on the comparison of experimental runs, the following can be stated:

In terms of ADP elements and ODP categories the lowest impacts are obtained with Run 1. For ODP Run 6 yields close results to Run 1.

For ADP fossil, AP, HTP, POCP and TETP impact categories, most favourable outcomes are got by Run 7.

On the other hand, lowest EP, FAETP, GWP and MAETP impacts are obtained by Run 5.

Therefore, depending on which impact categories are of importance, the decision-makers can choose the right alternative. If ADP elements and ODP categories are prioritized over others Run 1 with introducing 35.7 mg/l SPS and 1.340 kWh/m^3 energy input should be selected. In case ADP fossil, AP, HTP, POCP and TETP categories are important, a treatment alternative composed of 78.5 mg/l SPC and 0.670 kWh/m^3 energy input (Run 7) should be adopted. Finally, if EP, FAETP, GWP and MAETP categories rank more important, then Run 5 having 238 mg/l SPS introduction with 0.223 kWh/m^3 energy requirement should be applied.

At this stage it should be noted that along with prioritizing the environmental impacts of concern, decision makers also consider financial burdens of the treatment options. Figure 4 outlines the costs related evaluation for alternative runs. The costs given are comprised of chemical costs and cost of electricity.

As can be clearly seen from Fig. 4, Run 7 with the lowest ADP fossil, AP, HTP, POCP and TETP, yields the lowest operating cost. On the other hand, Run 5 where lowest EP, FAETP, GWP and MAETP levels are obtained, has

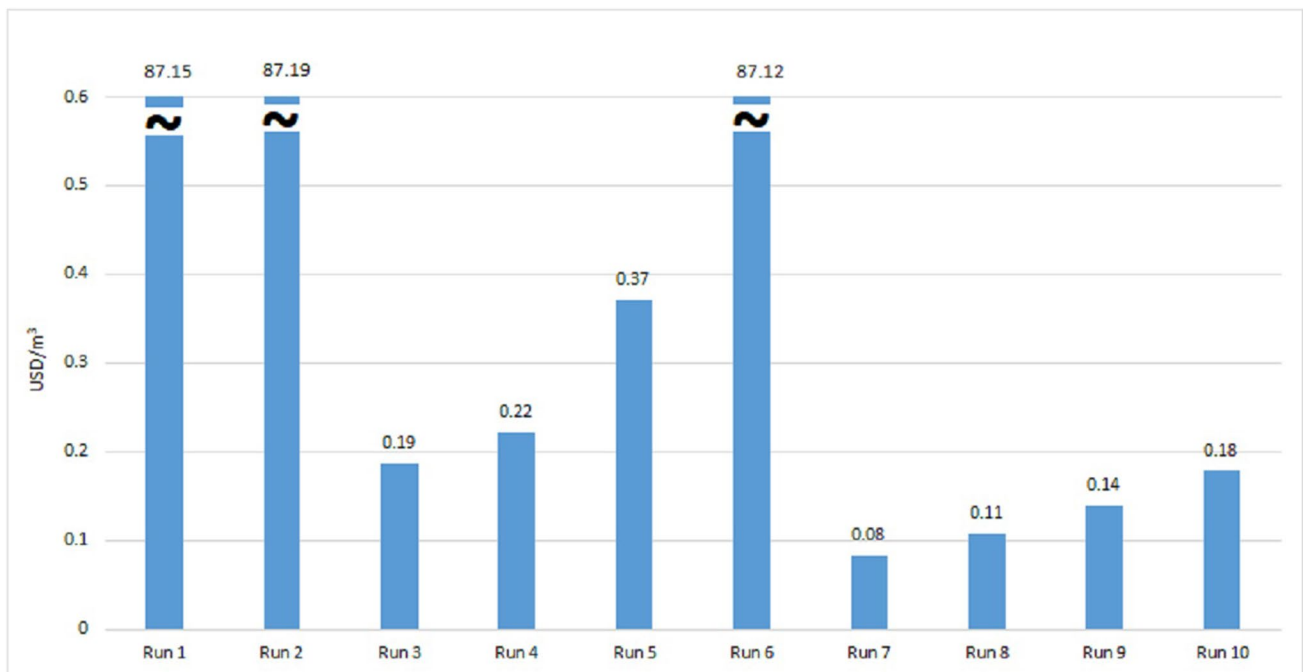


Fig. 4 Operating costs



an operating cost of 0.37 USD per treating a cubic meter wastewater.

A concise outline that shows the main reasons of getting environmental impacts for Run 1, 5 and 7 are stated in the following part.

ADP elements for Run 1 arises mainly due to non-renewable elements of copper (31%), cadmium and gold (both with 14% contribution) and lead (12%). ADP elements of Run 5 is of cadmium (20%), gold (19%), copper (15%) and lead (14%). Whereas ADP elements related to Run 7 is generated mainly because of copper and gold (each with 22% share).

ADP fossil for Run 1 is obtained mainly due to hard coal (40%), lignite (29%) and natural gas (25%) consumption. Petroleum and natural gas (each with around 32% contribution) and hard coal are producing the ADP fossil of Run 5. On the other hand, hard coal (36%), natural gas (30%) and lignite (22%) are the contributors to ADP fossil for Run 7.

AP is generated due to SO₂ and NO emissions for Runs 1, 5 and 7. The following contribution percentages for runs are obtained: Run 1: SO₂ (79%) and NO (18%); Run 5: SO₂ (81%) and NO (17%); Run 7: SO₂ (77%) and NO (19%).

Around 70, 56 and 63% of EP are generated due to phosphate emissions for Runs 1, 5 and 7, respectively.

FAETP of Runs 1, 5 and 7 are mainly caused by nickel, copper and beryllium emissions to water.

GWP, one of the most important environmental impact categories arise due to CO₂ emissions to atmosphere with more than 91% contribution for all the Runs 1, 5 and 7.

Selenium emissions to water is the main source of HTP for Runs 1 and 7. Whereas, arsenic and chromium (+ VI) emissions to atmosphere are the main reason of HTP for Run 5.

For Runs 1, 5 and 7, selenium emissions to water can be quoted as the main source of MAETP.

Halon and tetrachloromethane emissions to atmosphere are responsible for ODP of the runs.

SO₂ together with nitrous oxide emissions generate POCP for Runs 1, 5 and 7.

TETP arises mainly due to chromium (VI) emissions to soil.

Conclusion

This study concentrates on how to evaluate the treatability results with the sustainability assessment for a dye containing segregated textile stream. A segregated textile dyebath discharge that contains hydrolyzed Reactive Black

5 dye (RB5) is subjected to treatability tests with UV-C activated persulfate (PS) and UV-C activated percarbonate (PC) advanced oxidation processes. The outcomes yielding 100% RB5 (color; measured as peak absorbance) removal are further investigated through LCA to reveal the treatment alternative with minimal environmental impacts.

Based on the methodology adopted in this study, the application of the roadmap composed of the below given steps is recommended to find out the most environmentally sound treatment alternative with operating conditions:

- Running treatability studies
- Evaluating treatability results that yield the required efficiencies
- Based on laboratory studies, listing inputs and outputs for treatment alternatives yielding required efficiencies
- Running a modelling study through LCA methodology to find out the environmental impacts related to treatment alternatives
- Prioritizing environmental impact category/categories by considering their importance to decision-makers (eg. GWP for climate neutral actions)
- Cost assessment
- Addressing a treatment method and related operating conditions based on the prioritization of the environmental impacts and calculated costs.

The appraisal given in this study is based on laboratory scale treatability results. One should keep in mind that the impacts shown in the study will differ to some extent during scaling up to a full treatment plant. Nevertheless, the outcomes of this study yield a general comparative perspective on the environmental impacts of the treatment alternatives investigated.

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Declarations

Competing interests The authors declare that they have no competing interests.

Ethical approval This article does not contain any studies with human participants or animals performed by any of the authors.



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